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**ВЛИЯНИЕ ВЫГОРАЮЩЕГО ПОГЛОТИТЕЛЯ (Gd) НА  
КОЭФФИЦИЕНТ РАЗМНОЖЕНИЯ ( $k_{\infty}$ ) В ПРОЦЕССЕ  
ВЫГОРАНИЯ ТОПЛИВА ДЛЯ ПОЛНОМАСШТАБНЫХ И  
ПОЛИЯЧЕЕЧНЫХ МОДЕЛЕЙ ДЛЯ РЕАКТОРА ВВЭР**

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**Аннотация.** В статье рассмотрены различные концентрации выгорающего поглотителя (ПВ) гадолиния (Gd) в системе компенсации избыточной реактивности реактора типа ВВЭР при длительных кампаниях. Здесь проанализировано влияние метода на полномасштабную и полиячеечную модели размещения выгорающего поглотителя в топливе с гадолиниевыми стержнями (ТВЭГ). Показано сильное влияние состава выгорающего поглотителя (ПВ) в топливе с гадолиниевыми стержнями (ТВЭГ) на зависимость коэффициента выгорания топлива.

**Ключевые слова:** выгорающий поглотитель, компенсация, реактивность, полномасштабная модель, полиячеечная модель, коэффициент размножения, выгорание.

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## Introduction

The general methods available for reactivity control, the insertion and withdrawal of neutron absorbers, generally referred to as control rods, is the approach usually taken for power reactors. A burnable poison, (a nuclide that has a large neutron absorption cross section) or a chemical shim (a neutron-absorbing chemical, usually boric acid, which is dissolved in the moderator or coolant) is employed for reactivity control depending on reactor types. There are three methods to control the reactivity of a power plant. The first method (by the insertion and withdrawal control rod) has a negative effect on the axial power distribution, and the insertion or withdrawal control rod will change the power of reactor. The second method is chemical shim (a neutron-absorbing chemical, usually boric acid, which is

concentrated in the moderator or coolant), this method has a better effect on the radial and axial power distribution, but in depending on burnup, the concentration of boric acid in the moderator should be decrease by operator or automation system to conserve the criticality state and any mistake will happen in this system will cause accident in the core. The third method is burnable absorber [1-2] (a nuclide that has a large neutron absorption cross section), and there are many nuclides using in the fuel as an absorber like Gd, Pu, Cm, Np, Am and Th etc. All these elements change the reactivity of the power reactor.

### **Objective**

In operating WWER-1200 reactors, which use extended campaigns up to one and a half to two years, the number of fuels with gadolinium rod 18–24 pieces, and the weight content of  $Gd_2O_3$  is 5–8 wt.%. Due to this arrangement, the burnable absorber is permanent and completely disappears at the end of the campaign. In here evaluated the concentration of Gadolinium in the fuel with gadolinium rod (tveg) for the full-scale loading and poly cells model.

### **Description of the program GETERA-93**

The GETERA-93 program is designed for neutron-physical calculation of cells and poly-cells of nuclear reactors, both fast and thermal, in spherical, cylindrical and planar geometry. The program can be used to solve a wide range of problems: preparation of small-molecule cross sections for subsequent large-scale calculations, investigation of various characteristics of reactors in cell and poly-cellular models, solving problems related to burnout of fuels, modeling of various reactor regimes. The neutron-physical distribution of neutrons is calculated in the probability method of the first collisions [3-4].

The GETERA-93 program can be used to solve a wide range of tasks, both research and applied. With its help, it is possible to study the neutron-physical characteristics of the reactors at the cell and poly cells level. The algorithm for the multiplicity of the cell makes it possible to simulate sufficiently large fragments of the reactor on a small number of cells. In addition to calculations of the fragments of the reactor, the built-in algorithms allow modeling the burnup processes in the reactor and calculating the characteristics of fuel cycles: for example, the coarse fuel burnup in reactors with cyclic and in reactors with continuous fuel overload. Another large area of application of this program is the preparation of libraries of small sections so that they can later be used in full-scale models. The program allows you to take into account the environment of the cell when preparing sections, which is important when preparing the correct constants for small programs [5-6]. The program prepares both macromicro-sequences and constants for dynamic software complexes.

### **Full-scale and Poly-cells model**

Fuel assembly (FA) contains four types of rod

1. Fuel rod (tvel)
2. Fuel with gadolinium rod (tveg)
3. Central rod
4. Guide channel

Fuel rod and fuel with gadolinium rod (Figure-1) are divided into five zones. The first zone, which is contains «He» gas. The second zone, which is contains fuel ( $U^{235}$ ) (for the tvel) and fuel with gadolinium (for the tveg) [7-8]. The third zone which is contains clearance zone. Forth zone contains shell zone and the fifth zone is coolant zone.

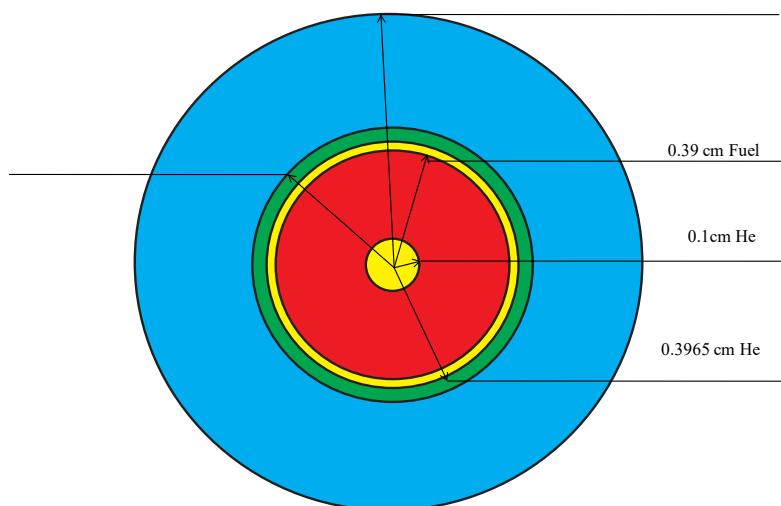


Figure 1 – Fuel zone (tvel) or Fuel with gadolinium (tveg) zone position in 0.39 cm radius

In Figure 2, it is shown that there are 312 rods in the fuel assembly. If  $n$  - fuel with gadolinium rod, then  $312 - n$  = fuel rods. In Russian WWER reactors, the ratio of the fuel with gadolinium (tveg) and fuel rods is - 1: 6, 1: 12, 1: 18 and 1: 24. So, 1: 6,  $N$  (Total) = (1+6) = 7,  $312 / 7 \approx 45$  fuel with gadolinium rods and  $(312 - 45) = 267$  fuel rods. In the same way, for the 1:12,  $N = 13$ ,  $312 / 13 \approx 24$  fuel with gadolinium rods and  $(312 - 24) = 288$  fuel rods, for the 1:18,  $N = 19$ ,  $312 / 19 \approx 17$  fuel with gadolinium rods and  $(312 - 17) = 295$  fuel rods, for the 1:24,  $N = 25$ ,  $312 / 25 \approx 12$  tags and  $(312 - 25) = 300$  fuel rods. In this calculation, we can say that the poly cells model is 1: 6, 1: 12, 1: 18 and 1: 24 and full-scale model is 45: 267, 24: 288, 17: 295 and 12: 300. [9-10]

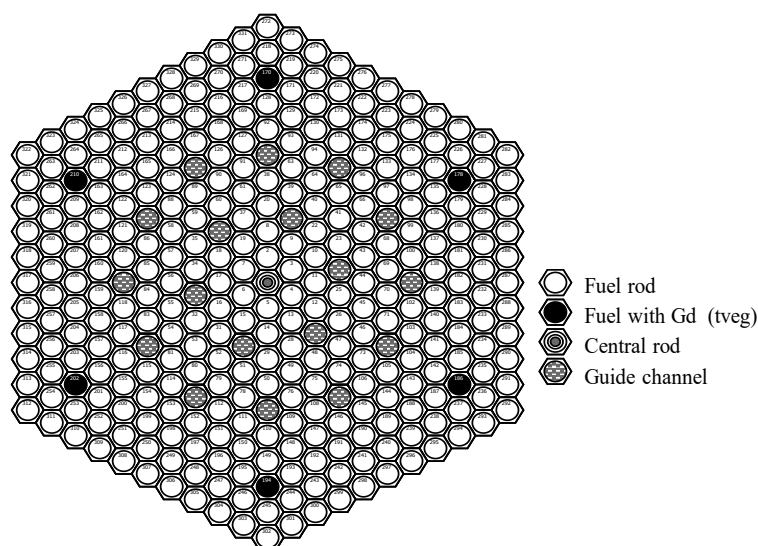


Figure 2 – 312 Fuel rods assembly

### Calculate the multiplying coefficient characteristic for the Full-scale and Poly cells model

For the full-scale fuel assembly (when 45 fuel with gadolinium rods and 267 fuel rods) and poly cells: (1 fuel with gadolinium rod and 6 fuel rods), then the multiplying coefficient vs time was calculated by the program GETERA-93 for the different (0.1%, 0.25%, 0.5%, 0.75% and 1%) concentration of gadolinium, which is shown in the figure 3a and figure 3b respectively. In here full-scale fuel assembly and poly cells are given the same result. [11-12]

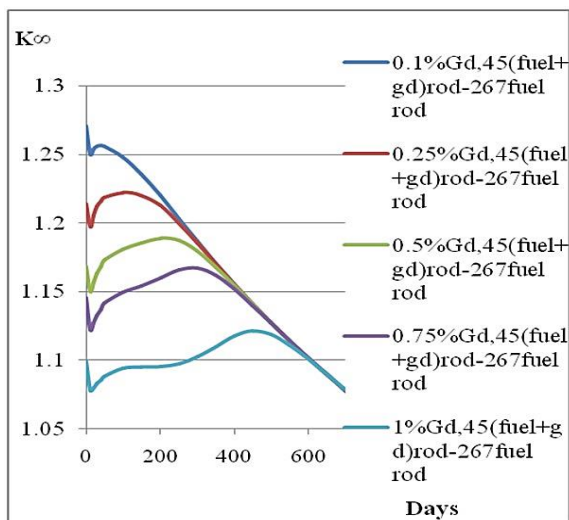


Figure 3a – Multiplying coefficient vs Days in full scale 45 (Fuel+Gd) rods and 267 fuel rods model

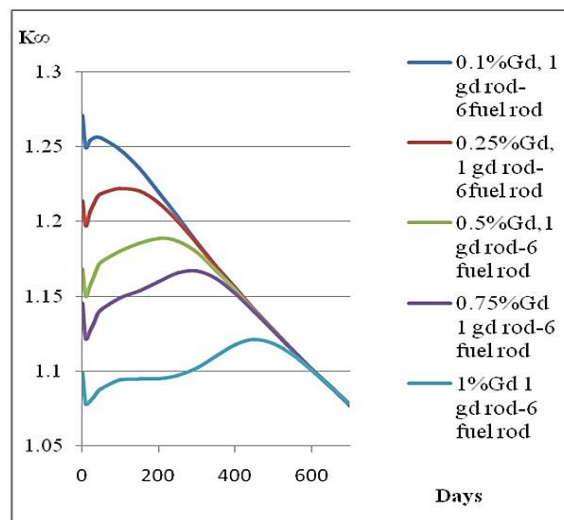


Figure 3b – Multiplying coefficient vs Days in full poly cells 1 (Fuel+Gd) rod and 6 fuel rods model

Graph analysis: When the concentration of gadolinium is 0.1% in the full-scale (45 tveg rods and 267 tvelrods) model, then the gadolinium rod (tveg) very soon (approximately 50 days) absorbed neutrons and after that only fuel  $U^{235}$  was burned. In the same way, when a little much more gadolinium 0.25% then approximately 100 day's gadolinium fuel rod absorbed neutrons, after that only fuel  $U^{235}$  was burned. In here it was seen that, more concentration of gadolinium absorbed neutrons for a long time until all gadolinium was burned, and then only fuel  $U^{235}$  was burned. Same result was shown in the poly cells model (fig. 3b).

When in the fuel assembly has 24 (Fuel+Gd) rods and 288 fuel rods for the full scale and poly cells 1 (Fuel+Gd) rod and 12 fuel rods, then the multiplying coefficient vs days shown in the figure 4a and figure 4b accordingly. But in here, 24 fuel with gadolinium rods which is less than <45 fuel with gadolinium rods. For this reason, for the concentration of (0.5%, 0.75%, 1.5% and 3%) gadolinium, 24 fuel with gadolinium rods absorbed neutrons for a long time and then burned fuel  $U^{235}$ .

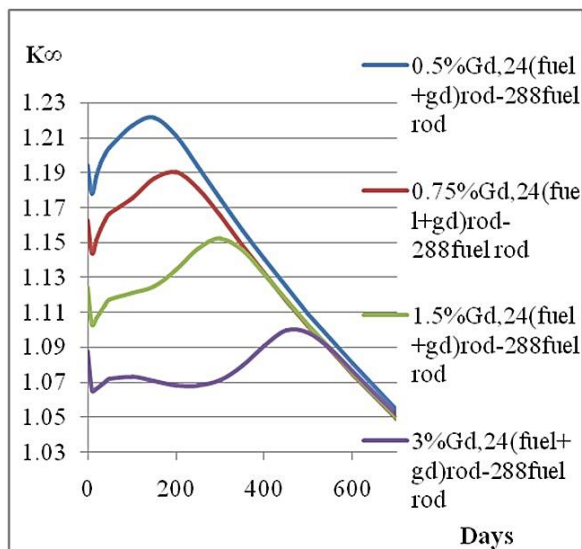


Figure 4a – Multiplying coefficient vs Days in full scale 24 (Fuel+Gd) rods and 288 fuel rods model

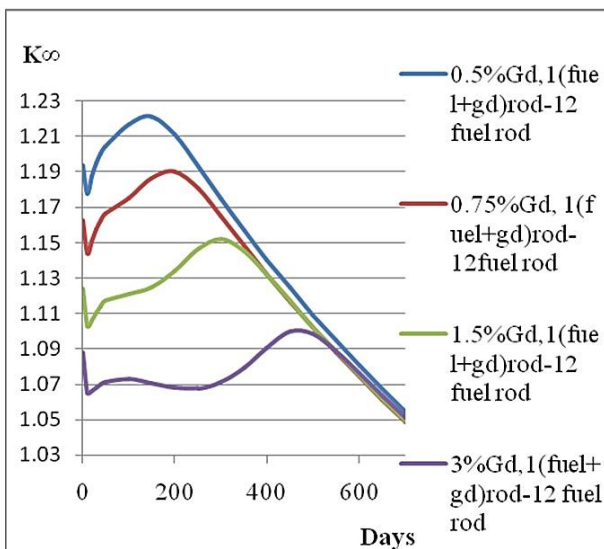


Figure 4b – Multiplying coefficient vs Days in poly cells 1 (Fuel+Gd) rod and 12 fuel rods model

For the fuel assembly 17 (Fuel+Gd) rods and 295 fuel rods and his poly cells 1 (Fuel+Gd) rod and 18 fuel rods, fuel assembly 12 (Fuel+Gd) rods and 300 fuel rods for the

full-scale model and his poly cells model 1 (Fuel+Gd) rod and 24 fuel rods was calculated by the program GETERA-93. Which is shown in figure 5a, 5b and 6a, 6b accordingly.

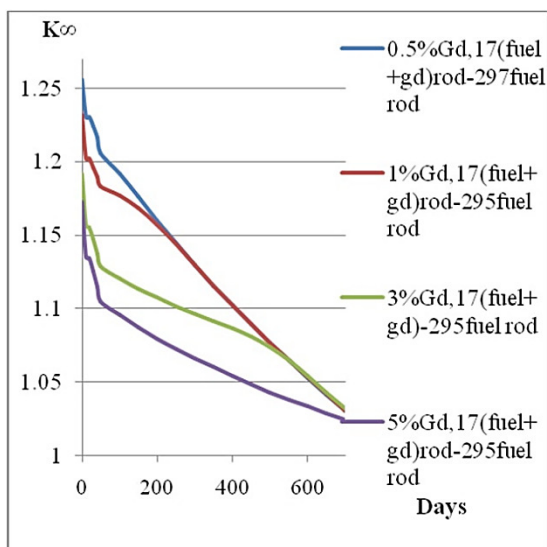


Figure 5a – Multiplying coefficient vs Days in full scale 17 (Fuel+Gd) rods and 295 fuel rods model

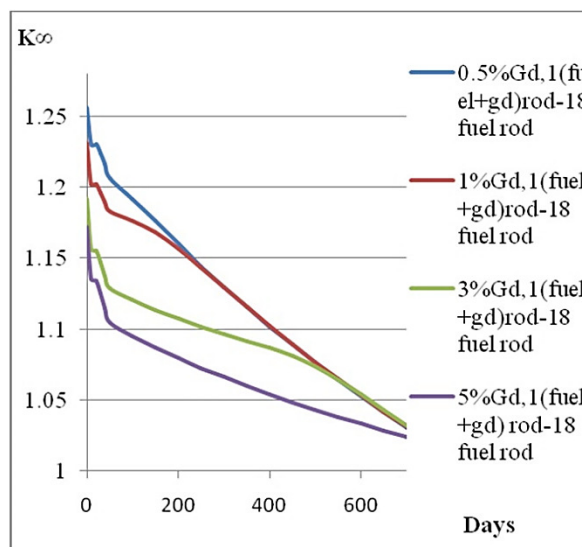


Figure 5b – Multiplying coefficient vs Days in poly cells 1 (Fuel+Gd) rod and 18 fuel rods model

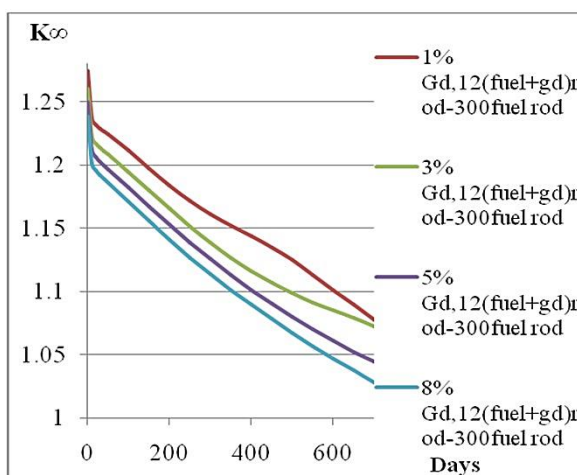


Figure 6a – Multiplying coefficient vs Days in full scale 12 (Fuel+Gd) rods and 300 fuel rods model

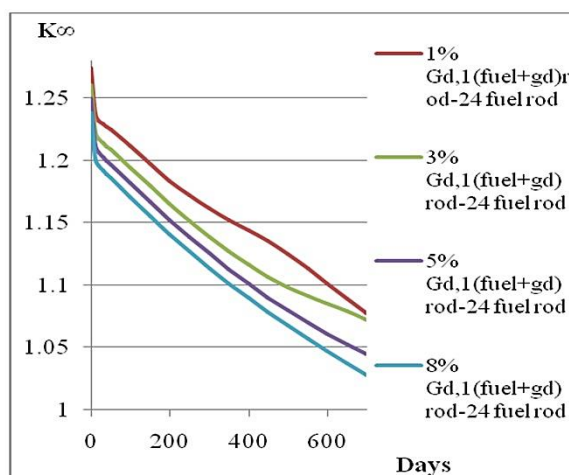


Figure 6b – Multiplying coefficient vs Days in poly cells 1 (Fuel+Gd) rod and 24 fuel rods model

Graph analysis: Figure 5a, 5b and 6a, 6b shows that, when in the full-scale has 17 (Fuel+Gd) rods, then absorption time is less than 12(Fuel+Gd) rods absorption time.

### Result

It is shown that the placement of a burnable absorber in a fuel assembly has both a quantitative and a qualitative effect on the change in the multiplication factor in the process of fuel burnup. It should also be noted that the duration of gadolinium burning depends on its amount and distribution inside the fuel assembly.

### Conclusion

Calculation results on a full-scale model of a WWER polycell simulating fuel assemblies with pin-by-pin nodalization showed that varying the amount and location of the burnable poison inside the fuel assemblies get possible to control the reactivity margin for

burnup and increase the efficiency of nuclear fuel usage in WWER reactors. Such problem is an optimization problem and can be solved by calculation.

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## Effect of the Burnable Absorber (Gd) on the Multiplying Coefficient ( $K_{\infty}$ ) in the Process of Fuel Burnup for Full-Scale and Poly Cells Models for the WWER Reactor

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**Abstract.** The paper considers various concentrations of burnable absorber (BA) Gadolinium (Gd) in the system of compensation of excess reactivity in the reactor of WWER type at the extended campaigns. It is analyzed the influence of the method for the Full-scale and Poly-cells model placing the burnable absorber in the fuel with gadolinium rods (tveg). The strong influence of the BAs composition in the fuel with gadolinium rods (tveg) dependence on the multiplication factor of the fuel burnup is shown.

**Keywords:** burnable absorber, compensation, reactivity, full-scale model, poly-cellular model, multiplication factor, burnup.

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